



## A two-step sensitivity analysis for hydrological signatures in Jinhua River Basin, East China

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Complete List of Authors:	Pan, Suli; Zhejiang University, Guangtao, Fu; University of Exeter Chiang, Yen-Ming ; Zhejiang University, Department of Hydraulic Engineering Ran, Qihua; Zhejiang University Xu, Yueping; Zhejiang University, Hydraulic Engineering
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**1. Author name and affiliations:**

Suli Pan<sup>a</sup>, Guangtao Fu<sup>b</sup>, Yen-Ming Chiang<sup>a</sup>, Qihua Ran<sup>a</sup> and Yue-Ping Xu<sup>a</sup>

<sup>a</sup> Institute of Hydrology and Water Resources, College of Civil Engineering and Architecture, Zhejiang University, Hangzhou, 310058, China

<sup>b</sup> Center for Water Systems, College of Engineering, Mathematics and Physical Sciences, University of Exeter, North Park Road, Harrison Building, Exeter, EX4 4QF, UK

**Full postal address and e-mail address:**

Suli Pan:

**Postal address:** Room B526, Anzhong Building, Campus Zijingang, Zhejiang University, No.388 Yuhangtang Road, Hangzhou, China. **E-mail:** pansuli@zju.edu.cn

Guangtao Fu:

**Postal address:** Center for Water Systems, College of Engineering, Mathematics and Physical Sciences, University of Exeter, North Park Road, Harrison Building, Exeter, EX4,4QF,UK. **E-mail:** G.Fu@exeter.ac.uk

Yen-Ming Chiang:

**Postal address:** Room B528, Anzhong Building, Campus Zijingang, Zhejiang University, No.388 Yuhangtang Road, Hangzhou, China. **E-mail:** chiangym@zju.edu.cn

Qihua Ran:

**Postal address:** Room B519, Anzhong Building, Campus Zijingang, Zhejiang University, No.388 Yuhangtang Road, Hangzhou, China. **E-mail:** ranqihua@zju.edu.cn

Yue-Ping Xu:

**Postal address:** Room B513, Anzhong Building, Campus Zijingang, Zhejiang University, No.388 Yuhangtang Road, Hangzhou, China. **E-mail:** yuepingxu@zju.edu.cn

**2. Corresponding author:**

**Yue-Ping Xu**

*Tel.:*+86 15924171902. *E-mail address:* [yuepingxu@zju.edu.cn](mailto:yuepingxu@zju.edu.cn) (Y-P Xu).

**Postal address:** Room B513, Anzhong Building, Campus Zijingang, Zhejiang University, No.388 Yuhangtang Road, Hangzhou, China.

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# A two-step sensitivity analysis for hydrological signatures in Jinhua River Basin, East China

Suli Pan<sup>a</sup>, Guangtao Fu<sup>b</sup>, Yen-Ming Chiang<sup>a</sup>, Qihua Ran<sup>a</sup> and Yue-Ping Xu<sup>a,\*</sup>

<sup>a</sup> Institute of Hydrology and Water Resources, College of Civil Engineering and Architecture, Zhejiang University, Hangzhou, 310058, China

<sup>b</sup> Center for Water Systems, College of Engineering, Mathematics and Physical Sciences, University of Exeter, North Park Road, Harrison Building, Exeter, EX4 4QF, UK

## Abstract

Parameter calibration and sensitivity analysis are usually not straightforward tasks for distributed hydrological models, owing to the complexity of model and large number of parameters. A two-step sensitivity analysis approach is proposed for analyzing the hydrological signatures based on the Distributed Hydrology-Soil-Vegetation Model in Jinhua River Basin, East China. A preliminary sensitivity analysis is conducted to obtain influential parameters via Analysis of Variance. These parameters are further analyzed through a variance-based global sensitivity analysis method to achieve robust rankings and parameter contributions. Parallel computing is designed to reduce computational burden. The results reveal that only a few parameters are significantly sensitive and the interactions between parameters could not be ignored. When analyzing hydrological signatures, it is found that water yield was simulated very well for most samples. Small and medium floods are simulated very well while slight underestimations happen to large floods.

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\* Corresponding author at: Institute of Hydrology and Water Resource, College of Civil Engineering and Architecture, Zhejiang University, room B513, Anzhong Building, No.388 Yuhangtang Road, Hangzhou 310058, China.

Tel.: +86 15924171902. E-mail address: [yuepingxu@zju.edu.cn](mailto:yuepingxu@zju.edu.cn) (Y-P Xu).

**Key words:** Sensitivity analysis, ANOVA method, Sobol’s method, Hydrological signature,  
DHSVM, Peak flow

**1 Introduction**

Distributed physically-based hydrological models have obtained ever-growing attention in recent decades owing to consideration of spatial variability and widely applications for ungauged basins (Razavi and Coulibaly 2012, Zhan *et al.* 2013, Palanisamy and Workman 2014, Noori *et al.* 2014, Noori and Kalin 2016). Applications of these models are wide, including impact analysis of climate change and land cover, runoff and flood forecasting, and improving insights of hydrological process (Du *et al.* 2012, Rahman *et al.* 2013, Xu *et al.* 2013, Tan *et al.* 2015, Winchell *et al.* 2015, Cao *et al.* 2016, Chen *et al.* 2016).

However, the applications of distributed hydrological models for these fields depend on the performance of model simulation, which is optimized by model calibration (Bittelli *et al.* 2010, Cibin *et al.* 2010). Hydrological models are characterized by a set of parameters, varying from simple lumped rainfall-runoff models with several parameters to sophisticated, distributed models with large numbers of parameters, even hundreds (Moradkhani and Sorooshian 2008). Therefore, manual calibration for distributed hydrological models with all parameters is time consuming and practically difficult to find optimal parameter sets. Likewise, a lack of identification for influential parameters in model simulation may cause waste of time on un-influential parameters (Bahremand and De Smedt 2008). Hence, it is very essential to identify the dominant parameters controlling model behavior, which contributes to raising calibration efficiency and obtaining more satisfactory simulation. One useful approach of dominant parameter identification is through implementation

of sensitivity analysis (SA), which can quantify the influence of parameters on model response (Wagener *et al.* 2001, Xu and Mynett 2006, Tang *et al.* 2007b, Zhang *et al.* 2013, Zhan *et al.* 2013, Song *et al.* 2015, Ren *et al.* 2016). The results of sensitivity analysis are helpful to determine sensitive parameters which should be paid more attention to in model calibration. A comprehensive comparison of various sensitivity analysis methods are implemented in literatures (Saltelli *et al.* 2000b, Saltelli *et al.* 2004, Tang *et al.* 2007b) and the results reveal that the Sobol's method is the effective method to obtain global parameter sensitivities. Furthermore, Tang *et al.* (2007a) applied the Sobol's method to a distributed hydrological model and obtained robust sensitivity rankings of the parameters, which could be able to significantly reduce the number of parameters for calibrating a hydrological model.

Hydrological signatures are often used to quantify hydrological input variables and response variables (Yadav *et al.* 2007, Westerberg and McMillan 2015). Signatures are widely used for catchment classification (Wagener *et al.* 2007, Sawicz *et al.* 2011), change detection (Archer and Newson 2002) and model calibration (Gupta *et al.* 2008). Yadav *et al.* (2007) adopted hydrological signatures (slope of the flow duration curve (FDC) and runoff ratio) and similarity indices for catchments classification. Hartmann *et al.* (2013a, 2013b) evaluated hydrological model performance with respect to hydrological signatures. Likewise, Westerberg *et al.* (2011) applied several points selected on FDC for model calibration and two selection methods are compared to estimate their impacts on parameter calibration. Furthermore, the application of hydrological signatures in hydrological modeling can offer meaningful information contained in hydrographs. Signatures could also help to interpret the relations between models and underlying hydrological processes and reflect various aspects of model behaviors.

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106       The Distributed Hydrology-Soil-Vegetation Model (DHSVM) (Wigmosta *et al.* 1994), a fully  
107 distributed hydrological model, is characterized by numerous parameters. It does not contain any  
108 sensitivity analysis or model calibration module. Therefore sensitivity analyses for DHSVM are  
109 often implemented using one-factor-at-a-time (OFAT) (Cuo *et al.* 2011), a local sensitivity test  
110 using stepwise, single parameter perturbation method (Du *et al.* 2014) and method of Morris  
111 (Kelleher *et al.* 2015). These SA methods are all simple or local and could not fully represent the  
112 relations between input parameters and model outputs due to their few sample sizes for lots of  
113 parameters and the interactions among parameters are often ignored. In this study, a two-step  
114 approach is therefore proposed for in-depth sensitivity analysis for DHSVM by adding two SA  
115 modules (Sobol's and Analysis of Variance (ANOVA) methods, and iterated fractional factorial  
116 design (IFFD) sampling approach is applied in ANOVA to reduce the computational burden) into  
117 the DHSVM model, which can provide robust sensitivity rankings and parameter's individual  
118 contributions, total contributions and interactions. Additionally, the parameters values for different  
119 soil and vegetation types are distinct in this study. In order to fully evaluate the performance of  
120 DHSVM, several hydrological signatures are selected in this study.

121       The structure of this paper is as follows. Section 2 describes the material and methods used in  
122 the study. Section 3 presents the results of two-step sensitivity analysis and analysis of  
123 hydrological signatures. Section 4 provides discussion concerning the two-step sensitivity analysis  
124 approaches and its further application in future. Section 5 summarizes the findings in this study.

## 125 2 Material and methods

### 126 2.1 Methodology framework

127 The methodology framework of this study is presented in Figure 1. The first step is to  
128 prepare input data for the hydrological model and determine ranges of nearly all parameters.  
129 ANOVA sensitivity analysis is then undertaken to obtain preliminary sensitive parameters in the  
130 first step. This is because that model outputs are assumed to be normally distributed. Substantial  
131 departures from the assumption of normality can affect sensitivity analysis results (Lindman,  
132 1974) and the results of ANOVA sensitivity analysis may not be robust. Therefore, only the  
133 effect of individual parameters is adopted in the study. Additionally, the number of model runs in  
134 ANOVA method is smaller than that in the Sobol's method used in the second step. These  
135 preliminary sensitive parameters from ANOVA are further analyzed via Sobol's method to  
136 achieve robust results, including effects of individual parameters and interactions between  
137 parameters. Afterwards, final sensitive parameters and their interactions are quantified and  
138 ranked. The third step is to interpret the impact of final sensitive parameters on model simulation  
139 through considering objective functions, sensitivity index and values of parameters. The fourth  
140 step is to execute hydrological signature analysis and percentile analysis for peak flows for  
141 samples with efficiency criteria  $> 0.7$ . Moreover, detailed signatures analysis and percentile  
142 analysis are done for selected individual samples.

143 **Figure 1.** Methodology framework used in this study.

144 2.2 Study area

145 Jinhua River, a tributary of Qiantang River, is located in the Midwest of Zhejiang Province,  
146 East China (Figure 2). This river has a length of 195 km and the catchment area is 6 782 km<sup>2</sup> (Xu  
147 *et al.* 2015). In this study, the basin above Jinhua hydrological station is included and its  
148 catchment area is 5 996 km<sup>2</sup>, which is appropriate to apply DHSVM model (the model is mainly  
149 applicable to watersheds whose area is less than 10 000 km<sup>2</sup>). Also this model has been  
150 successfully used in the study area (Xu *et al.* 2015). The prevailing climate of the basin is Asian  
151 subtropical monsoon, which is characterized by abundant precipitation and high temperature in  
152 summer and rainless and cold winter. The annual average temperature is 17 °C. The elevation  
153 ranges from 29 to 1 296 m in the basin (Figure 3). The annual mean precipitation is 1 424 mm.  
154 More than 50% of the annual total precipitation happens in the period from May to July. Because  
155 of the unevenly temporal distribution of precipitation, Jinhua River Basin suffers a lot from  
156 droughts and floods. Good hydrological simulation will provide support to disaster prediction  
157 and prevention, and sustainable river management. Figure 2 also presents the locations of five  
158 meteorological stations and the hydrological station used in the study.

159 **Figure 2.** Location of the six stations used in the study.

160 2.3 Overview of DHSVM

161 Distributed Hydrology-Soil-Vegetation Model (DHSVM) (Wigmosta *et al.* 1994, Wigmosta  
162 and Burges 1997, Wigmosta *et al.* 2002) is a physically-based distributed hydrological model.  
163 DHSVM provides an integrated representation of hydrology-vegetation dynamics at the spatial  
164 scale identified by digital elevation map (DEM) data (the spatial resolution is typically 10-200



m). The river basin is separated into computational grid cells depending on DEM. Soil and vegetation characteristics are allocated to each computational grid cell. At each time step, DHSVM offers simultaneous solution to water and energy balance equations for every grid cell in the river basin. The hydrological connection of individual grid cell is realized by surface and subsurface flow routing. The spatial and temporal resolutions are 200 m and daily respectively. The version 3.1.1 of DHSVM is adopted in this study.

DHSVM consists of seven modules, i.e., evapotranspiration, snowpack accumulation and melt, canopy snow interception and release, unsaturated moisture movement, saturated subsurface flow, surface overland flow and channel flow (Wigmosta *et al.* 2002). Evapotranspiration is presented adopting a two-layer canopy model with both two layers divided into wet and dry areas. Modules concerning snow, i.e., snowpack accumulation and melt and canopy snow interception and release, are not considered here owing to the fact that snow is rare in the study area. Unsaturated moisture movement with multiple root zone soil layers is assessed utilizing Darcy's Law (Domenico and Schwartz 1988). Every grid cell exchanges available water with its adjacent grid cells using a function of its hydraulic conditions bringing about a transient, three-dimensional formulation of saturated subsurface flow and surface flow. DHSVM adopts a cell-by-cell method to route saturated subsurface flow utilizing a kinematic or diffusion approximation (Wigmosta *et al.* 1994, Wigmosta and Lettenmaier 1999). Grid cells in the basin are centered on each DEM point.

Surface runoff is routed by a unit hydrograph method or an explicit cell-by-cell method (the explicit cell-by-cell approach is adopted in this study). Surface runoff occurs in a cell when meeting any of the following conditions: firstly, the available water in grid cell exceeds the

187 defined infiltration capacity; secondly, the water table exceeds the ground surface. The  
188 downslope movement of surface runoff is based on a cell-by-cell mode which is similar to the  
189 approach applied for subsurface flow. Flow in stream channels and road drainage ditches is  
190 routed by utilizing a cascade of linear channel reservoirs. Roads are not considered in this study  
191 owing to the fact that detailed road information is not available and the area percentage of roads  
192 is very small compared to the big basin area. However, it is kept in the mind that roads often  
193 generate overland flow from compacted surfaces, intercept subsurface flow at road cuts and alter  
194 hillslope hydrologic processes. Ignoring the roads may affect the accuracy of hydrological  
195 simulation, in particular peak and peak time. In the model, lateral inflow to a channel segment,  
196 from the cells which it passes through, is composed of subsurface flow and overland flow  
197 intercepted by channels.

198 Generally, DHSVM parameters can be classified into elevation, stream, road, soil and  
199 vegetation categories. Parameters related to the characteristics of stream network such as stream  
200 segment length, width and aspect are determined based on the DEM data. That is to say, these  
201 parameters do not need to be calibrated. Soil/vegetation parameters such as field capacity need to  
202 be calibrated if its real value in physical meaning is not known or no observation is available.  
203 The calibration of vegetation and soil parameters in DHSVM is very common in other studies  
204 (Thanapakpawin *et al.* 2007, Safeeq and Fares 2012, Cuartas *et al.* 2012).

205 *2.4 Model input data*

206 The climate data including average air temperature, wind speed, relative humidity, sunshine  
207 duration and precipitation from five meteorological stations, i.e., Jinhua, Dongyang, Wuyi,

Yongkang and Yiwu (Figure 2), are available in this study. The climate data is obtained from Zhejiang Provincial Metrological Administration. The incoming shortwave radiation and longwave radiation are calculated using climate data. The observed runoff at Jinhua hydrological station is obtained from Zhejiang Provincial Hydrology Bureau (Figure 2). The time period of climate and runoff data is from 1991-2000.

The other data needed for DHSVM include watershed boundary (mask), digital elevation map (DEM), soil type, vegetation type, soil depth and streams network. The DEM data (Figure 3) with a resolution of 90 m are downloaded from the Shuttle Radar Topography Mission (SRTM) website (<http://srtm.csi.cgiar.org/>). Considering computational burden, the resolution of DEM is redefined to 200 m in the model. The water boundary is determined based on DEM. The soil data (Figure 3) are obtained from Nanjing Institute of Soil Research, China. According to the USDA (United States Department of Agriculture) soil texture classification system needed in DHSVM, the soil classes are reclassified. The vegetation data (Figure 3) are obtained from WESTDC Land Cover Products 2.0 (2006) (<http://westdc.westgis.ac.cn>). Table 1 shows vegetation and soil classes and their percentages in Jinhua River Basin. The soil depth and streams network are generated based on DEM and mask using Arc Workstation.

**Figure 3.** DEM (digital elevation map) (a) soil distribution (b) and vegetation distribution (c) in Jinhua River Basin.

**Table 1.** Vegetation and soil classes and their percentages in Jinhua River Basin.

### 2.5 Analysis of Variance (ANOVA) sensitivity analysis

For this study, Analysis of Variance (ANOVA) is adopted to determine the preliminary sensitive parameters in DHSVM simulation owing to its popularity and common application (Steel

and Torrie 1988, Shinohara *et al.* 2016). In this method, parameters are sorted into specific scope of parameter values indicating intervals with same parameter value width. Based on ANOVA terminology, inputs are referred to as “factor” and values of factors are referred to as factor levels. Moreover, output is called “response variable”. ANOVA method was proposed by Fisher (1925). The  $F$  value is a key statistic in ANOVA and describes the statistical significance of differences in the mean responses among the levels of corresponding parameter. Therefore, the  $F$  values are utilized to judge whether parameter causes difference in response variable, i.e. sensitivity. The higher the  $F$  value is, the more crucial parameter is. Then, the parameter is more sensitive in model simulation. The equation of  $F$  value is described as follows:

$$F = \frac{\bar{S}_A}{\bar{S}_E} \tag{1}$$

Where  $\bar{S}_A$  is referred to group (treatment) mean squares from factor  $A$ , which reflects the differences between mean value of samples in different levels and mean value of all samples.  $\bar{S}_E$  is referred to error (residual) mean squares, which reflects the differences between value of each sample and mean value of samples in different levels.

One-way ANOVA is used to evaluate the significance of one factor on response variable. Two-way ANOVA is dealt with two or multiple factors and applied to determine the single effect of factor and interaction effects between factors. No assumption is demanded regarding the functional form of relationships between the outputs and the inputs in ANOVA. Generally, ANOVA method could apportion the variance, but substantial departures from the assumption of normality can affect analysis results (Lindman, 1974). Therefore, only the effect of individual parameter is adopted in the study.

ANOVA will become computationally infeasible if the number of input is large. The number

of model runs could be decreased and computational efficiency will be much higher by using IFFD sampling approach (Saltelli *et al.* 1995, Andres 1997). In IFFD, parameters are sampled at three different levels (groups): low, middle and high, rather than from a continuous range (Saltelli *et al.* 1995). These discrete levels are defined equally within the original parameter scope. The use of a slight number of factor levels empowers the sampling formula to achieve results effectively and accurately (Andres 1997). In Jinhua River Basin, there are ten vegetation classes and six soil classes. The number of parameters is more than 200, if all soil and vegetation classes are included. Because there is hardly any snow in the study area, parameters concerning snow are excluded in sensitivity analysis. Moreover, soil and vegetation classes are only chosen when their area percentages in the basin are higher than 10%. Thus, the vegetation and soil classes in italic script in Table 1 are selected. In total, three soil classes, i.e., sandy loam (SL), loam (L) and clay loam (CL), and three vegetation classes, i.e., mixed forests (MF), grasslands (GL) and cropland (CrL) are finally considered in ANOVA sensitivity analysis. The total percentages for selected soil and vegetation classes are about 90%. Consequently, in ANOVA sensitivity test, the number of parameters is 83 and the sample size is 14 000. According to Cuo *et al.* (2011), model simulation is sensitive to both vegetation height and vegetation minimum resistance. Different parameter ranges are used for these vegetation parameters in different vegetation stories (as shown in Table 2, italic). Ranges, unit and abbreviation of selected parameters are presented in Table 2. Besides, monthly LAI in different months is distinguished via appropriate multipliers and the ranges of LAI in Table 2 are represented for January which has the minimum LAI.

**Table 2.** Ranges, unit and abbreviation of constant, soil and vegetation parameters for ANOVA sensitivity analysis.

272 2.6 Sobol's sensitivity analysis

273 Sobol's sensitivity analysis method (Saltelli *et al.* 2000a, Sobol' 2001), a variance-based  
274 method, is selected in this study for in-depth global sensitivity analysis since this method is able  
275 to quantify not only the contributions of individual parameter to DHSVM simulation but also  
276 their interactions, which could not be obtained accurately from ANOVA (Zhang *et al.* 2013, Xu  
277 *et al.* 2014). In addition, sensitivity index provided by the Sobol's method are more effective  
278 than other sensitivity analysis methods for its capability of describing the interactions between a  
279 large number of variables for extremely nonlinear models, such as distributed hydrological  
280 models (Tang *et al.* 2007a, Tang *et al.* 2007b, Rajabi *et al.* 2015). In this method, the attribution  
281 of total output variance to individual model parameters and their interactions can be defined as  
282 follows (Bois *et al.* 2008):

283 
$$V = \sum_i (V_i) + \sum_{i < j} (V_{ij}) + \sum_{i < j < m} (V_{ijm}) + \cdots + (V_{1,2,\dots,k}) \quad (2)$$

284 Where  $V$  is the total variance of model output;  $V_i$  is the first order variance for the  $i$ th  
285 variable  $x_i$ ;  $V_{ij}$  is the interaction variance between  $x_i$  and  $x_j$ ;  $k$  is the total number of input  
286 variables. The variances displayed in Equation (2) can be assessed by approximate Monte Carlo  
287 numerical integrations. The sensitivity of individual parameters or their interactions,  
288 i.e. sensitivity index are calculated according to their contribution in the total variance  $V$ .

289 First order sensitivity index  $S_i = \frac{V_i}{V} \quad (3)$

290 Second order sensitivity index  $S_{ij} = \frac{V_{ij}}{V} \quad (4)$

291 Total order sensitivity index  $S_{Ti} = \frac{\sum_i (V_i) + \sum_{i < j} (V_{ij}) + \sum_{i < j < m} (V_{ijm}) + \cdots + (V_{1,2,\dots,k})}{V} \quad (5)$

292 Where  $S_i$  is the first order sensitivity index corresponding to the input factor  $x_i$ ; the second

order sensitivity index  $S_{ij}$  evaluates the interactions between  $x_i$  and  $x_j$ ; the total order sensitivity index  $S_{Ti}$  calculates the total effects of the input factor  $x_i$  on the model simulation.

## 2.7 Objective function and parallel computing

The proper choice of an objective function is often demanded for evaluating the performance of a hydrological model in sensitivity analyses and model calibration, but not essential (Hartmann *et al.* 2015, Pianosi *et al.* 2016). Objective function must be able to accurately express the distance between observation and simulation. Comprehensive objective functions and efficiency criteria have been used in hydrological simulation (Rao and Han 1987, Yan and Haan 1991). In the study, Nash-Sutcliffe efficiency ( $NS$ ) is firstly selected.  $NS$  is a normalized statistic that confirms the relative difference of residual variance in contrast to observation variance (Nash and Sutcliffe, 1970).  $NS$  is calculated as shown in Equation (6).  $NS$  is more sensitive to peak flows than low flows because squared deviations is utilized which leads to the possibility that low flows is not accurately simulated by hydrological models (Schaeffli and Gupta 2007, Criss and Winston 2008, Muleta 2012, Hartmann *et al.* 2015).  $E_{rel}$  (Equation (7)) is a statistic which is widely applied to evaluate the performance of low flow simulation (Krause *et al.* 2005, Raposo *et al.* 2012). The combination with equal weights ( $NE$ ; Equation (8)) is then used as the final objective function in this study. The relevant equations are shown as follows:

$$NS = 1 - \frac{\sum_{i=1}^n (O_i - S_i)^2}{\sum_{i=1}^n (O_i - \bar{O})^2} \quad (6)$$

$$E_{rel} = 1 - \frac{\sum_{i=1}^n \left( \frac{O_i - S_i}{O_i} \right)^2}{\sum_{i=1}^n \left( \frac{O_i - \bar{O}}{\bar{O}} \right)^2} \quad (7)$$

$$NE = 0.5 \times NS + 0.5 \times E_{rel} \quad (8)$$

Where  $O_i$  is referred as the observed streamflow;  $S_i$  is referred as the simulated streamflow;  $\bar{O}$  is referred as the average of observed streamflow.

DHSVM runs relatively slowly. The meteorological data used in this study are from 1991 to 2000 at daily scale data. The cell grid is 200m and the basin area is 5 996 km<sup>2</sup>. Therefore, each run of model will take about 50 minutes under Linux server. The run time of DHSVM is 486 days in ANOVA sensitivity analysis with a sample size of 14 000. Similarly, the run time is 708 days in Sobol's sensitivity analysis with a set of 20 400 samples. Computer cluster consisting of five PCs with same configurations is used in this study and the logistical setup of computer cluster is a master-slave distribution. In other words, one PC plays as master and assigns tasks to slaves, i.e., the other four PCs. The slaves receive and finish the tasks from the master. Moreover, in order to decrease the run interval, the master also participates in running task as well as slaves. And the configuration in PC is single-CPU (central processing unit) with four cores. Moreover, Hyper-Threading (with Hyper-Threading, one physical core appears as two processors to the operating system) is installed in five PCs and the number of processors is then forty. The softwares which are necessary to be set up in five PCs include gcc, g++, NFS (File Share System), SSH (Secure Shell) and MPI (Message Passing Interface). The parallel pattern in this study is data-parallel. That is to say, the tasks for slaves and master are running model based on the sample sets generated by sensitivity analysis methods, and the process of generating sample sets is done on the master. The run intervals of ANOVA and Sobol's sensitivity analyses are 13 days and 18 days respectively via parallel computing. The computational efficiency has been greatly enhanced after parallel computing.



## 2.8 Hydrological signatures

Hydrological signatures are able to investigate the simulation effect of hydrological models more comprehensively and thoroughly (Yadav *et al.* 2007, Yilmaz *et al.* 2008, Winsemius *et al.* 2009). To analyze the performance of different aspects of streamflow simulated via DHSVM, five distinct conditions of hydrological signatures are selected, including average flow conditions, low flow conditions, peak flow conditions, duration of flow events for low flow conditions and duration of flow events for peak flow conditions (Olden and Poff 2003, Bormann *et al.* 2011, Westerberg and McMillan 2015, Shafii and Tolson 2015). The specific hydrological signatures of different conditions are described in Table 3, i.e., mean annual runoff for average flow conditions, low flow signature and base-flow signature for low flow conditions, specific mean annual maximum flows for peak flow conditions, annual minimum of 1-/3-/7-/30-d means of daily runoff and annual maximum of 1-/3-/7-/30-d means of daily runoff for duration of flow events. The detailed abbreviation, unit and definition are shown in Table 3.

**Table 3.** Description of the six hydrological signatures used in the study.

In order to evaluate the performance of simulation results conveniently, a new criterion ( $P$ ) is used and can be calculated by Equation (9). The value of hydrological signatures for observed streamflow is constant. However,  $P$ -value of simulated streamflow changes depends on each parameter set.

$$P = \frac{HS(Q_{sim})}{HS(Q_{obs})} - 1 \quad (9)$$

Where  $HS(Q_{obs})$  is referred as the value of hydrological signature for observed streamflow;

$HS(Q_{sim})$  is referred as the value of hydrological signature for simulated streamflow.

As shown in Equation (9), if  $P > 0$ , the value of hydrological signature for simulated

streamflow is higher than that of observed streamflow, indicating that the simulated signature is overestimated. On the contrary, the simulated signature is underestimated. The lower the absolute value of  $P$  is, the higher performance of hydrological model is.

As described in Section 2.1, Jinhua River Basin suffers a lot from floods. Besides the peak-related hydrological signature shown in Table 3, peak flows extracted from observed and simulated runoff are compared via percentiles. Here, Peak-over-threshold (POT) (O'Brien *et al.* 2015, Hirsch and Archfield 2015, Mallakpour and Villarini 2015) is adopted to select peak flows. For POT method, the choice of the threshold is important. If the threshold is too low, excessive number of peak flows is selected. On contrary, only a few peak flows are considered when the threshold is too high. In this study, mean of observed daily runoff (1991-2000) is used. Two subsequent peak events ( $P_1$  and  $P_2$ ) are identified as independent when the following two conditions are satisfied (Lang *et al.* 1999):

$$\begin{cases} \theta > 5 + \log(Area) \\ X_{\min} < \left(\frac{3}{4}\right) \min(P_1, P_2) \end{cases} \quad (10)$$

Where  $\theta$  is the interval of two subsequent peak events (days);  $Area$  is the area of watershed (miles<sup>2</sup>);  $X_{\min}$  is the minimum runoff during interval of two subsequent peak events (m<sup>3</sup>/s).

Based on these independent conditions and selected threshold, peak flows are extracted from the observed and simulated runoff in the study period (1991-2000).

### 375 3 Results

#### 376 3.1 ANOVA sensitivity analysis result

377 Figure 4 presents the  $F$ -value and percentage of the total variance at a significance level of  
 378  $p=0.05$ . Sixteen sensitive parameters are preliminarily selected from all parameters (83) of  
 379 DHSVM, based on the criterion that  $F$ -Value is bigger than 3.0. The sum of variance percentages  
 380 of selected sixteen parameters is about 97.6%. The higher the  $F$ -value is, the more sensitive the  
 381 parameter is.

382 Figure 4 shows that  $F$ -values of some parameters exceed three orders of magnitude larger  
 383 than 3.0. Hence, a threshold of 300 is adopted to determine whether a parameter is highly  
 384 sensitive or not. There are three highly sensitive parameters, i.e., rain LAI multiplier ( $R_j$ ),  
 385 porosity of clay loam ( $\phi(CL)$ ) and field capacity of clay loam ( $\theta_{fc}(CL)$ ), accounting for 19.3%,  
 386 9.6% and 40% of total variance respectively. Among these highly sensitive parameters, field  
 387 capacity of clay loam is the most sensitive parameter and its  $F$ -value is 1 583.4 which is far  
 388 larger than the threshold 300. Field capacity together with root zone depth ( $D(CrL)$ ) determines  
 389 realistic storage of available water in soil, and realistic storage will diminish with the decrease of  
 390 field capacity. Consequently, the same amount water access soil subsurface layers will have  
 391 higher runoff with decreasing field capacity. However, porosity together with root zone depth  
 392 decides the capacity of water in soil. Simulated peak flows will decrease and routing time will  
 393 increase with increasing porosity. Rain LAI multiplier is LAI multiplier for rain interception,  
 394 which will influence interception storage and evaporation.

395 Thirteen sensitive parameters are presented in Figure 4, including five soil parameters

(mainly from clay loam) and eight vegetation parameters (related to mixed forests and croplands). Understory minimum resistance ( $UR_{min}(MF)$ ) and overstory minimum resistance ( $OR_{min}(MF)$ ) of mixed forest are sensitive parameters. According to Wigmosta *et al.* (2002), canopy resistance is calculated separately for the understory and overstory. Similarly, understory height ( $Uh(MF)$ ) of mixed forest is sensitive to simulated streamflow. Additionally, in reality, the actual values for understory and overstory height of mixed forest are different. Vegetation height is related to aerodynamic resistance, which determines the rate of potential evaporation with other parameters. Vegetation minimum resistance, vapor pressure deficit ( $Ec(CrL)$ ) and soil moisture threshold ( $\theta^*(CrL)$ ) are used to calculate canopy resistance, which directly impact vegetation transpiration. LAI affects the capacity of canopy interception and acquisition of solar radiation. Therefore, the rate of potential evaporation will increase with increasing LAI. Lateral conductivity ( $K(CL)$ ) is used in the calculation of lateral flow movement and lateral conductivity exponential decrease ( $f(CL)$ ) describes exponent decrease of lateral conductivity with soil depth. Both of them influence the amount of lateral flow and routing time. Wilting point ( $\theta_{wp}(CL)$ ,  $\theta_{wp}(L)$ ) and bulk density ( $\rho_B(CL)$ ) are related to soil evaporation.

**Figure 4.** ANOVA parameter sensitivities based on the *NE* measure (*F*-value > 3).

Figure 5 shows the observed and simulated hydrographs (when the value of *NE* is the maximum in ANOVA sensitivity analysis) of 1994, 1995 and 1996, which correspond to moderate, wet and dry year respectively. The efficiency criteria for *NS*, *E<sub>rel</sub>* and *NE* (1991-2000 years) are 0.83, 0.81 and 0.82 respectively, which show a good performance of the hydrological model. In addition, the bias is -7.8%, which is well within the range -25%~25% (Safeeq and Fares 2012, Xu *et al.* 2015). However, the runoff, especially peak flow, is slightly underestimated.

In general, the simulation demonstrates that DHSVM is able to simulate river flows in a good way. Also it can be observed from Figure 5 that the model performance in the dry year (1996) is better than that in the moderate year (1994).

**Figure 5.** Model performance in 1994, 1995 and 1996 (corresponding to moderate, wet and dry year, respectively) when the value of  $NE$  ( $NS$ ,  $E_{rel}$  and  $NE$  are 0.83, 0.81 and 0.82 respectively) is the maximum in ANOVA sensitivity analysis.

### 3.2 Sobol's sensitivity analysis results

The input factors for Sobol's sensitivity test are preliminary sensitive parameters selected by ANOVA (as shown in Figure 4 and Table 4). As shown in Table 4, sixteen model parameters are considered in Sobol's sensitivity analysis and a sample size of 20 400 is used (according to Saltelli and Tarantola (2002), this sample size is appropriate). Saltelli (2000a) extended the Sobol's original work by adding special transformation to the randomly sampled parameters to reduce computational complexity. This transformation is used in this study and the ranges of porosity, field capacity and wilting point of clay loam are slightly changed (Italic in Table 4). The value of  $NE$  ranges from 0.2 to 0.88. Percentage of samples with  $NE$  value higher than 0.8, is up to 66.7%. Percentage of  $E_{rel}$  that is larger than 0.8 accounts for nearly 60% and the highest value of  $E_{rel}$  is 0.93. Moreover, a majority of samples has a value of  $NS$  higher than 0.7. In addition, biases are also calculated for all samples, and nearly all values are within the acceptable range of -25%~25% (Safeeq and Fares 2012). The percentage of correlation coefficient value higher than 0.9 is nearly 97%.

The total order sensitivity index is shown in Figure 6. Total order sensitivity index of 16 parameters range from 0.00 to 0.29. According to Tang *et al.* (2007b), parameters are highly

439 sensitive when the sensitivity indices are higher than 0.1 and sensitive with the indices higher  
440 than 0.01. Parameters are insensitive to streamflow simulation when its total order sensitivity  
441 index is smaller than 0.01. Figure 6 shows that there are eight highly sensitive parameters,  
442 including one constant parameter (rain LAI multiplier), four soil parameters (lateral conductivity,  
443 porosity, field capacity and wilting point of clay loam), and three vegetation parameters  
444 (understory monthly LAI, understory minimum resistance and root zone depths of croplands).  
445 Compared with the results from ANOVA sensitivity test, it shows that the identified parameters  
446 are similar and the ranking of them is compatible. Moreover, the most sensitive parameter in  
447 both methods is field capacity of clay loam. The role of field capacity ( $\theta_{fc}(CL)$ ) is dominant in  
448 unsaturated moisture movement module. In DHSVM model, no unsaturated flow is allowed to  
449 occur when the moisture content is below the field capacity. Unsaturated flow will increase with  
450 decrease of field capacity. The amount of runoff is obviously impacted by the value of field  
451 capacity. The higher the value of field capacity is, the more runoff will generate. In other words,  
452 more runoff could be obtained by decreasing the value of field capacity. Root zone depth ( $D(CrL)$ )  
453 has significant impacts on unsaturated flow, soil evaporation and the amount of moisture in the  
454 soil column. Model simulation is also highly sensitive to wilting point ( $\theta_{wp}(CL)$ ) and understory  
455 LAI ( $ULAI(CrL)$ ), owing to the fact that both of them play important roles in canopy resistance  
456 and evapotranspiration. As shown in Figure 3 and Table 1, the area percentage of forests/mixed  
457 forests is 34.7% (5.0%+0.1%+29.6%), and the area percentage only with understory is 64.5%  
458 (1.2%+22.9%+0.4%+36.7%+3.3%). It is easy to overlook that forests/mixed forests also have  
459 understory. Additionally, the mixed forest in the study area mainly consists of grasslands,  
460 shrublands and trees. The area percentage of trees in the mixed forest is about 30%, or less.

Moreover, the vegetation overstory parameters only have slight impacts on canopy interception and vegetation transpiration. This is an explanation for the conclusion that vegetation parameters related with overstory are less sensitive to model simulation.

**Table 4.** Ranges, number and abbreviation of parameters for Sobol's sensitivity analysis.

**Figure 6.** Sobol's total order sensitivity index based on the *NE* measure.

Interactions between parameters, i.e., second order sensitivity index, are presented in Figure 7. These interactions could not be identified with other local sensitivity analysis methods, such as OFAT (One-factor-at-a-time). The x-axis and y-axis are parameter numbers shown in Table 4. The constant parameter, rain LAI multiplier, has interactions with other fifteen parameters as shown in the first column of Figure 7. However, all sensitivity indices are smaller than a threshold value of 0.01, i.e., insensitive interactions. The interactions among field capacity of clay loam and other parameters are important. The second order sensitivity index between field capacity of clay loam and understory monthly LAI of croplands is the maximum and the value reaches 0.03. The total order sensitivity index of field capacity of clay loam reaches 0.29, which is much larger than its first order sensitivity index (0.18). As presented in Figure 3, clay loam and croplands covered most areas of the study area. In DHSVM model, LAI has direct effects on three crucial hydrological processes, i.e., vegetation canopy rainfall interception, evaporation and soil transpiration. LAI affects acquisition of solar radiation and is used as a multiplier in canopy precipitation interception. And the rate of potential evaporation will increase with the increase of LAI and available water into soil will then decrease. Moreover, field capacity is used to determine the realistic storage of available water in soil. Hence, the streamflow simulation is proven to be sensitive to the interactions between these parameters.

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4 483 In addition, the interactions between field capacity of clay loam and root zone depth of  
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6 484 croplands are also sensitive, for the reason that field capacity determines plant available water in  
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8 485 soil with root zone depth ( $D(CrL)$ ). The interactions increase the value of total order sensitivity  
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10 486 index of root zone depth to 0.27. Similarly, the interactions between field capacity of clay loam  
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12 487 and soil moisture threshold of croplands are also sensitive. The total sensitivity index of soil  
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14 488 moisture threshold reaches to 0.07, which is much larger than its first order sensitivity index  
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16 489 (0.03). This is due to the fact that soil moisture threshold also has an impact on transpiration of  
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18 490 soil like LAI. Understory height affects evaporation and transpiration of vegetation. This  
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20 491 explains the strong interactions between field capacity and understory height. Likely, the reason  
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22 492 for that model simulation is sensitive to the interactions between field capacity and vapor  
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24 493 pressure deficit is owing to the fact that vapor pressure deficit has an impact on evaporation and  
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26 494 transpiration of vegetation. In addition, vegetation minimum resistance affects water balance and  
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28 495 vegetation transpiration. Both wilting point and LAI have a significant influence on evaporation  
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30 496 of soil. So their interactions are sensitive to model simulation.  
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38 **Figure 7.** Interactions among sixteen parameters based on the *NE* measure.  
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41 498 *3.3 Hydrological signatures*  
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44 499 Six representative hydrological signatures from four flow conditions are selected in this  
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46 500 study. Evaluation criterion *P*-value shown in Equation (9) is used to analyze the performance of  
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48 501 the hydrological model based on hydrological signatures. Figure 8 shows the boxplots of  
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50 502 *P*-values for four hydrological signatures of all samples used in Sobol's sensitivity analysis, i.e.,  
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52 503 mean annual runoff (*AI*), Low flow signature (*LI*), Base-flow signature (*L2*) and Specific mean  
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annual maximum flows (*HI*). For hydrological signature *AI*, *P*-values range from -1.0 to 0.4. However, the *P*-values between 1% and 99% percentiles are totally within the acceptable scope (-25%~25%), which illustrates that the overall performance of *AI* is good. For hydrological signatures *L1*, approximately 96% of *P*-values are bigger than 25%, that is to say, the percentage for *P*-value within the acceptable range is only 4%. A number of samples are good with the *P*-value of *L2* close to zero. All of *P*-values of *HI* are lower than zero and 15.8% of *P*-values of *HI* are within the acceptable scope.

**Figure 8.** Boxplot for *P*-value of hydrological signatures (*A1* (Mean annual runoff), *L1* (Low flow signature), *L2* (Base-flow signature); and *H1* (Specific mean annual maximum flows)) of all samples in Sobol's sensitivity analysis.

In order to better understand the performance of the model concerning the four hydrological signatures in some specific samples, four samples with the value of *NE* higher than 0.7 are selected from all samples in Sobol's sensitivity analysis. Four samples, i.e., *Sample A*, *Sample B*, *Sample C* and *Sample D*, are selected according to the distinct intervals of *NE* value shown in Table 5. *Sample A* has the maximum value of *NE*. The results are displayed in Table 6. For *Sample A*, *P*-value of *AI* is -0.10 and that of *L1*, *L2* and *HI* are 0.68, -0.35 and -0.29 respectively. This explains that a high value of efficiency criteria could not guarantee good performance in all aspects of a hydrograph. For *Sample B*, hydrological signature *L1* (0.07) is close to zero and *AI* (-0.23) also within the acceptable range. *L2* (-0.54) and *HI* (-0.30) indicate less satisfactory simulations of base flow and peak flow. Nevertheless, base flow is reasonably simulated with *L2* (0.09) in *Sample C*, so is mean annual runoff (*AI* is equal to 0.01). For *Sample D*, peak flow is excellently simulated with *HI* (-0.22). Taking the total order sensitivity index (Section 3.2) and corresponding parameter values in *Sample A* into account, high value of porosity (0.58) and field

capacity (0.39) in clay loam result in the inferior performance of hydrological signature *L1*, *L2* and *H1*.

**Table 5.** Selected samples based on the *NE* value.

**Table 6.** Hydrological signatures of the observed and the simulated from selected samples and corresponding *P*-values.

Other hydrological signatures *DH1-4* and *DL1-4* of four selected samples are displayed in Figure 9 and Figure 10 respectively. For *DH1*, all four samples underestimate annual maximum of 1-day means of daily runoff in 1991-2000. As shown in Figure 9, the ranking of performance in *DH1* is *Sample D* > *Sample A* > *Sample B* > *Sample C*. This ranking is similar to that of hydrological signature *H1*. Underestimation is greatly improved in *DH2*. For *DH3*, four selected samples perform very well in 1991-2000. For *Sample D*, runoff is mostly overestimated with minor degrees in all years in *DH4*, which corresponds to hydrological signature *A1* with 0.21 of *P*-value. Different to *DH1-3*, the ranking of *DH4* is that *Sample C* is the best, *Sample A* is the second, *Sample B* is the third and *Sample D* is the last. And the ranking of *DH4* is similar to that based on hydrological signature *A1*.

**Figure 9.** Hydrological signature *DH1-4* for observed and simulated runoff from four selected samples as shown in Table 5.

As presented in Figure 10, for *DL1*, *Sample B* simulates very well in all years. However, other three samples underestimate *DL1* during most years. This ranking is totally similar to that of hydrological signature *L1*. The overestimation is improved for four samples in *DL2*. For *DL3*, performance of four samples is further better than *DL1* and *DL2*. By comparing the meaning of *DL3* and *L2*, it is reasonable that the ranking of *DL3* is the same to *L2*. The ranking of *DL4* is similar to that based on hydrological signature *A1*.

Hydrological signatures *DH1-4* and *DL1-4* represent maximum and minimum annual flow

of various durations, which describe the performance of duration of flow event in model simulation and provide important insights into a hydrograph. As shown in Figure 9 and Figure 10, the performance of four selected samples in *DH1* and *DL1* is not ideal. However, performance of *DH3* and *DL3* is good, which illustrates annual maximum and minimum of 7-day means of daily runoff are reasonably simulated.

**Figure 10.** Hydrological signature *DL1-4* for observed and simulated runoff for four selected samples as shown in Table 5.

Besides six hydrological signatures described above, peak flow percentile is further used to explore the performance of peak flow simulation. Figure 11 shows the peak flow percentiles for the observed and selected samples. These samples are from Sobol's sensitivity analysis samples and chosen with *NS* higher than 0.7. As presented in Figure 11,  $Q_{s-1}$  (1<sup>th</sup> percentile flows) –  $Q_{s-70}$  (70<sup>th</sup> percentile flows) are simulated reasonably. However, Figure 11 also shows that extreme peak flows (with percentile larger than 0.75) are not well simulated which is corresponding to the performance of hydrological signature *H1* and streamflow curve shown in Figure 5.

**Figure 11.** Peak flow percentiles for observed and simulated runoff from samples whose *NS* > 0.7 in Sobol's sensitivity analysis.

In order to understand the performance of peak flow simulation in individual samples, three samples are selected based on the *NS* value instead of *NE* value (Considering the fact that the maximum value of *NS* is 0.85 and *NS* should be bigger than 0.7, three not four distinct intervals are identified). Three samples, i.e., *Sample PA* (maximum value of *NS*), *Sample PB* and *Sample PC*, are selected according to various intervals of *NS* value shown in Table 7. The results are shown in Figure 12. For *Sample PA*,  $Q_{s-1}$  –  $Q_{s-25}$  is simulated very well. However, the other peak flow percentiles are underestimated in *Sample PA*. The reason for this is the high value of field

capacity (0.38) and low value of wilting point (0.07) of clay loam. For *Sample PB*,  $Q_{s-1}$ -  $Q_{s-75}$  exhibits slight overestimation. *Sample PC* performs better than the others,  $Q_{s-1}$ -  $Q_{s-70}$  is totally consistent to  $Q_{o-1}$ -  $Q_{o-70}$  and  $Q_{o-75}$  -  $Q_{s-99}$  shows less underestimation.

**Table 7.** Selected samples for peak flow based on the *NS* value.

**Figure 12.** Peak flow percentiles for observed and simulated runoff from three selected samples as shown in Table 7.

**4 Discussion**

It is common to apply one sensitivity analysis method to hydrological models and identify dominant parameters in hydrological model simulation. However, the proposed framework in this study provides a means to identify parameter sensitivities of DHSVM by using a two-step sensitivity analysis approach. In the first step, the ANOVA method was used to identify preliminary sensitive parameters in the DHSVM model simulation. This is because model outputs are assumed to be normally distributed, which may cause the results of ANOVA sensitivity analysis not robust. Therefore, only the effect of individual parameters is adopted in the first step. The ANOVA method was actually used here as a screening sensitivity analysis method. Then these preliminary sensitive parameters identified by ANOVA were further analyzed via the Sobol's method to achieve robust results, including effect of individual parameters and interactions between parameters in the second step. In the end, the performance of the model was investigated for different parameter sets based on hydrological signatures. As we explained before, our aim here is to mainly provide parameter identification results for further calibration and validation. However, we believe during this sensitivity analysis stage, checking how the different parameter sets play a role in model simulation (through hydrological

signature analysis) can also be interesting.

In the two-step sensitivity analysis approach, the Sobol's method can apportion the variance in model output (streamflow) to the variance in the model parameters and meanwhile consider interactions among parameters. The results demonstrated that field capacity of clay loam is the most important, showing the largest total order sensitivity index and high value of interactions with other parameters. Others sensitive parameters include rain LAI multiplier affecting evaporation, lateral conductivity and porosity of clay loam contributing to streamflow simulation, and wilting point of clay loam affecting soil evaporation. Highly sensitive vegetation parameters consist of understory monthly LAI of croplands influencing evaporation, understory minimum resistance of croplands strongly affecting water balance and root zone depths of croplands influencing soil evaporation. These results are in good agreement with that of Du *et al.* (2014) who showed that vegetation LAI, minimum resistance, porosity, rain LAI multiplier, wilting point and field capacity are important parameters in the simulation of water yield in northern Idaho, USA, using a stepwise, single parameter perturbation method. Cuo *et al.* (2011) also concluded that lateral saturated hydraulic conductivity, porosity, minimum resistance and LAI should be given special attentions during model calibration based on One-factor-at-a-time (OFAT). Meanwhile, other literatures have studied parameters sensitivities of DHSVM to model simulation as well (Surfleet *et al.* 2010, Kelleher *et al.* 2015). Nevertheless, the sensitivity analysis methods used in these studies could only obtain single contribution of parameters or less robust sensitivity results. The Sobol's method is able to achieve robust sensitivity rankings and, what's more, the interactions between parameters. In particular, in the current study, the interactions between field capacity of clay loam and other parameters cannot be ignored. As

shown in Figure 6, the total order sensitivity index becomes 0.29, which is much larger than the first order sensitivity index (0.18) after considering the interactions. This study demonstrates that the Sobol's method did provide valuable information to parameter selections in DHSVM calibration, and promote further guides in searching for optimal parameter sets for this model through considering parameter interactions.

In this study, several soil and vegetation types whose area percentages are bigger than 10% were considered in the two-step sensitivity analysis. Simplified soil and vegetation classes in the sensitivity analysis for DHSVM model may have an impact on simulation results (Cuo *et al.* 2011, Surfleet *et al.* 2010, Du *et al.* 2014). For instance, it is obvious that model simulation will be affected if same values were set for overstory vegetation LAI of evergreen needleleaf forests and evergreen broadleaf forests. Likewise, it is unrealistic that same values were set for field capacity of clay and sand.

It should be noted that four hydrological signatures could not be well simulated simultaneously in any individual sample from Sobol's sensitivity analysis. Hence, in order to obtain better model simulation, multi-objective calibration is necessary to achieve optimal parameter sets. Considering the complexity of model and large number of parameters, manual calibration is inefficient and difficult to obtain global optimal parameter sets. Automatic calibration is preferred for DHSVM with parallel computing to reduce computational burden. Traditional calibration is usually performed with a single objective (Guo *et al.* 2014, Wang and Brubaker 2015). However, a single objective is often inadequate to meet multiple requirements (Vrugt *et al.* 2003). Efficient global optimization algorithms are therefore recommended for use to reliably search for the global optimal parameter sets (Zhang *et al.* 2013, Ye *et al.* 2014).

Peak flow is slightly underestimated in the model simulation of DHSVM. The possible reasons for this are from various dimensions. Firstly, model structural problems related to peak flow generation mechanism may exist in DHSVM, including that preferential flow was not considered in this study and the assumption that understory vegetation (if it exist) covers the entire cell in evapotranspiration mode. Secondly, only limited meteorological stations and daily scale data are used in the study. According to Booij (2003, 2005), the spatial and temporal variability of precipitation will affect the hydrological simulation. As shown in the test application from Wigmosta *et al.* (1994), the best time step of meteorological data for model simulation is 3-hour. Additionally, determination of appropriate resolution of DEM may be critical for model simulation. According to Dubin and Lettenmaier (1999), simulations of peak flow and runoff process are greatly impacted by DEM resolution. Safeeq and Fares (2012) also concluded that underestimation of the peak flows exist when modeling runoff of a Hawaiian watershed.

## 5. Conclusion

In this study, a two-step sensitivity analysis approach was used. Firstly, the sensitivity of nearly all parameters in DHSVM which was built for Jinhua River Basin, East China, was roughly analyzed via ANOVA. Sobol's sensitivity analysis method, a variance-based global sensitivity analysis method, was then applied to analyze the contributions of the preliminary influential parameters identified by ANOVA to streamflow simulation, including single contributions, total contributions and interaction contributions. Parallel computing was applied to reduce the computational burden. For all samples from Sobol's sensitivity analysis, performances

656 of hydrological signatures were also investigated. Additionally, peak flows extracted from the  
657 observation and simulation via POT approach were compared. The key findings of this study are  
658 summarized below:

659 (1) According to the Sobol's method, only a few number of model parameters are significantly  
660 sensitive in Jinhua River Basin, including a constant parameter (rain LAI multiplier), four  
661 soil parameters (lateral conductivity, porosity, field capacity and wilting point of clay  
662 loam), and three vegetation parameters (understory monthly LAI, understory minimum  
663 resistance and root zone depths of croplands). More attention should be paid to these  
664 parameters in future model calibration.

665 (2) The interactions between parameters cannot be ignored. For example, the total order  
666 sensitivity index of field capacity of clay loam reaches to 0.29, which is much larger than  
667 the first order sensitivity index (0.18) after considering the interactions between field  
668 capacity of clay loam and other parameters.

669 (3) High value of the objective function (*NE*) didn't indicate excellent performance of  
670 hydrological signatures. For most samples from Sobol's sensitivity analysis, water yield  
671 was simulated very well via DHSVM. However, minimum and maximum annual daily  
672 runoffs were underestimated in a majority of samples. And most of seven-day minimum  
673 runoffs were overestimated. However, good performances of these three signatures still  
674 exist in a number of samples.

675 (4) The model performances of specific individual samples in percentile analysis were  
676 summarized. Considering sensitive parameters together with their values, the good  
677 performance of maximum annual daily runoff in *Sample D* is owing to the low values of



rain LAI multiplier, understory monthly LAI and root zone depth. Likewise, *Sample PC* has the best performance in that its small, medium and large floods show less underestimation than others.

(5) Percentiles of peak flows extracted from the observed and simulated runoff indicate that small and medium floods were simulated reasonably. Slight underestimations happen to large floods. This is possibly due to the shortcomings of model structure and insufficient meteorological data used in the study.

(6) The work in this study helps further multi-objective calibration of DHSVM model and indicates where to improve to enhance the reliability and credibility of model simulation. Good simulation of the complete hydrograph is useful for water resources management, flood prediction and forecasting. Furthermore, the two-step sensitivity analysis approach can be applied to detailed parameter identification for model simulation with numerous parameters. The limitation of this approach lies in its demand for a large number of model runs.

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- 906 **Table 1.** Vegetation and soil classes and their percentages in Jinhua River Basin.
- 907 **Table 2.** Ranges, unit and abbreviation of constant, soil and vegetation parameters for ANOVA sensitivity analysis.
- 908 **Table 3.** Description of the six hydrological signatures used in the study.
- 909 **Table 4.** Ranges, number and abbreviation of parameters for Sobol's sensitivity analysis.
- 910 **Table 5.** Selected samples based on the *NE* value.
- 911 **Table 6.** Hydrological signatures of the observed and the simulated from selected samples and corresponding *P*-values.
- 912 **Table 7.** Selected samples for peak flow based on the *NS* value.
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- 915 **Figure 1.** Methodology framework used in this study.
- 916 **Figure 2.** Location of the six stations used in the study.
- 917 **Figure 3.** DEM (digital elevation map) (a) soil distribution (b) and vegetation distribution (c) in Jinhua River Basin.
- 918 **Figure 4.** ANOVA parameter sensitivities based on the *NE* measure ( $F$ -value  $> 3$ ).
- 919 **Figure 5.** Model performance in 1994, 1995 and 1996 (corresponding to moderate, wet and dry year, respectively) when the
- 920 value of *NE* (*NS*,  $E_{rel}$  and *NE* are 0.83, 0.81 and 0.82 respectively) is the maximum in ANOVA sensitivity analysis.
- 921 **Figure 6.** Sobol's total order sensitivity index based on the *NE* measure.
- 922 **Figure 7.** Interactions among sixteen parameters based on the *NE* measure.
- 923 **Figure 8.** Boxplot for *P*-value of hydrological signatures (*A1* (Mean annual runoff), *L1* (Low flow signature), *L2* (Base-flow
- 924 signature): and *H1* (Specific mean annual maximum flows)) of all samples in Sobol's sensitivity analysis.
- 925 **Figure 9.** Hydrological signature *DHI-4* for observed and simulated runoff from four selected samples as shown in Table 5.
- 926 **Figure 10.** Hydrological signature *DLI-4* for observed and simulated runoff from four selected samples as shown in Table 5.
- 927 **Figure 11.** Peak flow percentiles for observed and simulated runoff from samples whose *NE*  $> 0.7$  in Sobol's sensitivity
- 928 analysis.
- 929 **Figure 12.** Peak flow percentiles for observed and simulated runoff from three selected samples as shown in Table 7.

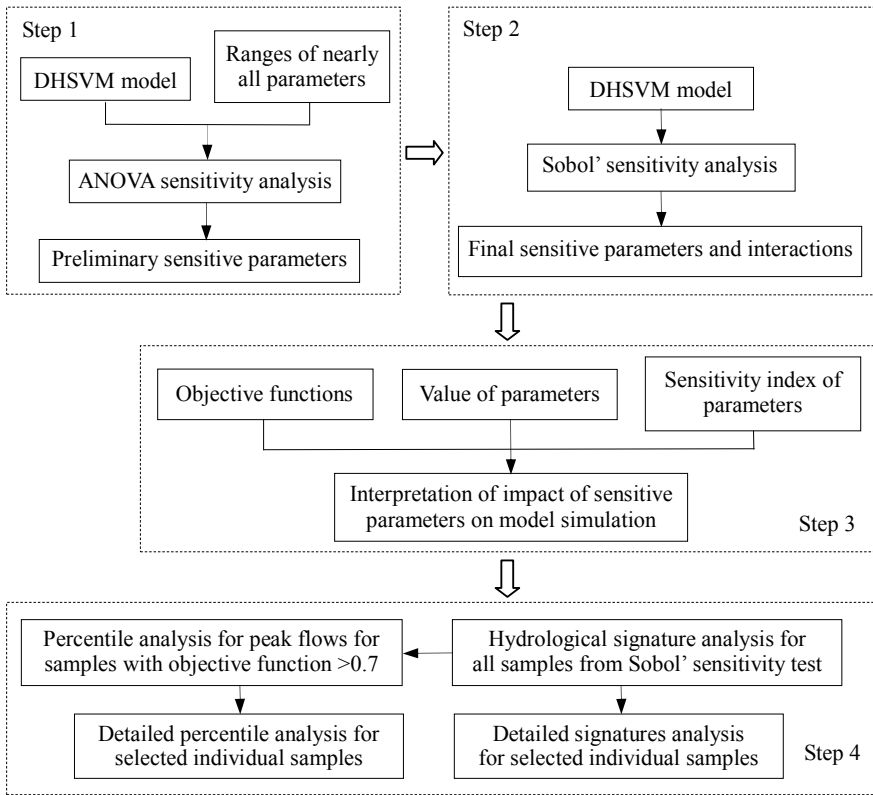


Figure 1. Methodology framework used in this study.

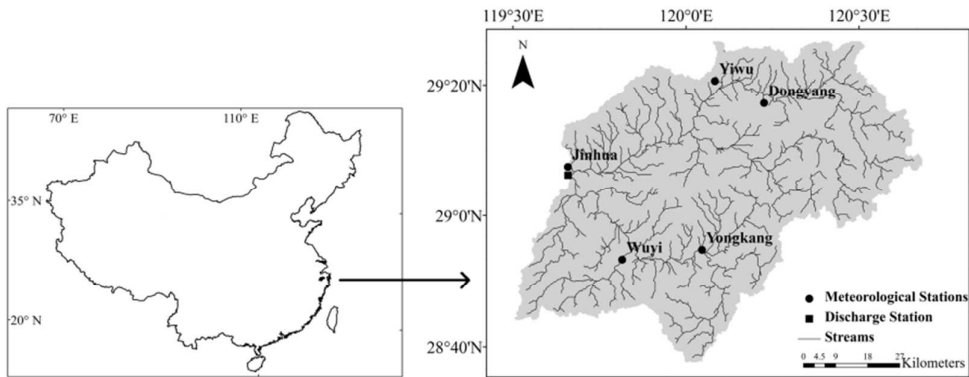


Figure 2. Location of the six stations used in the study.



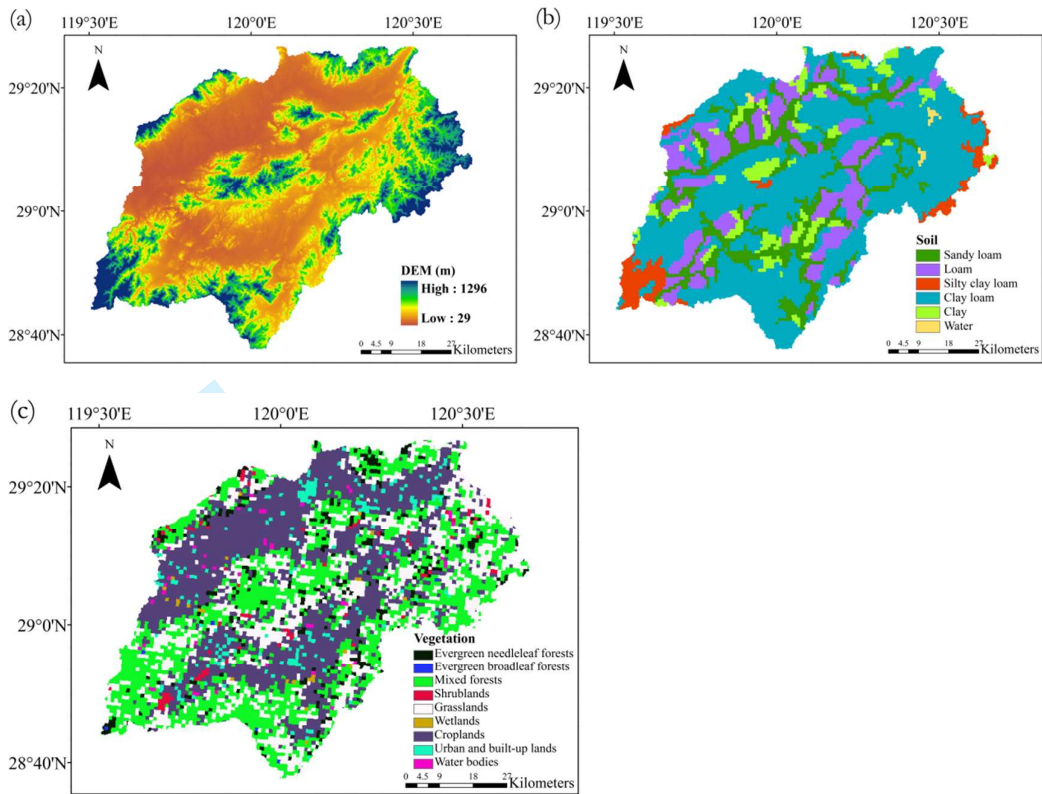


Figure 3. DEM (digital elevation map) (a) soil distribution (b) and vegetation distribution (c) in Jinhua River Basin.

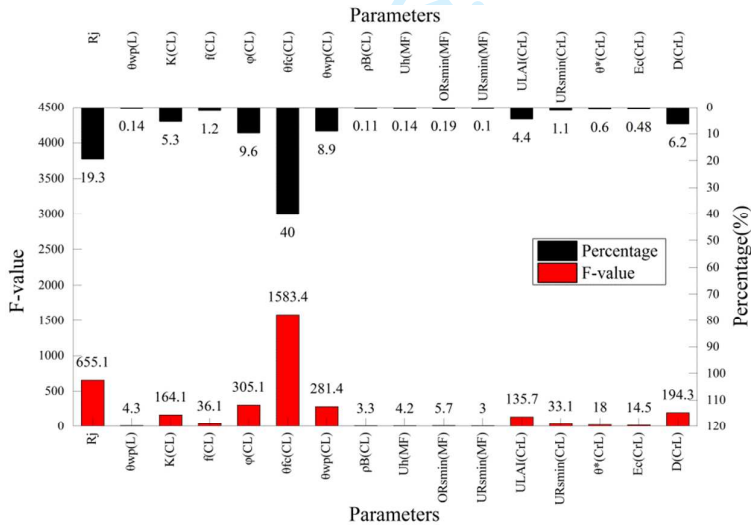
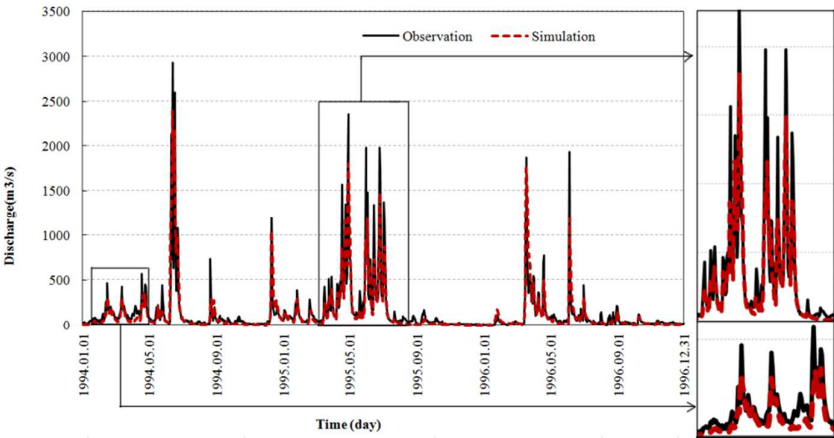
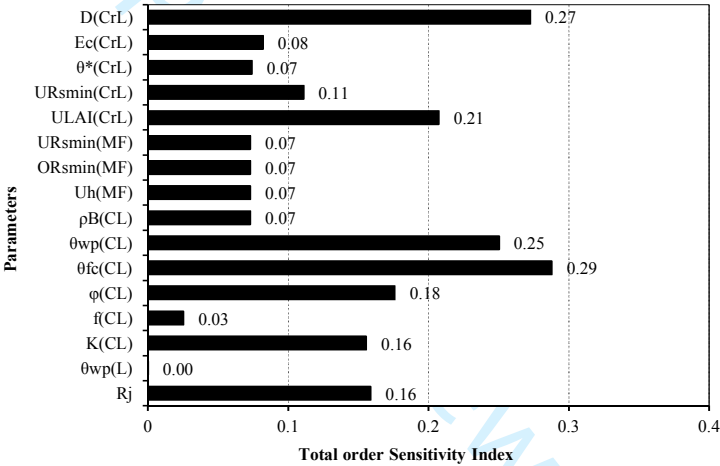


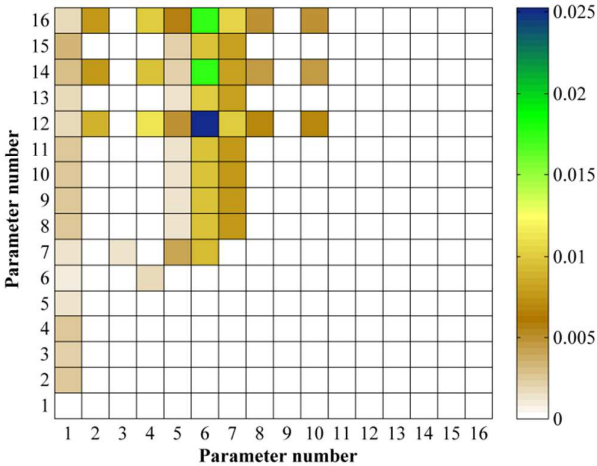
Figure 4. ANOVA parameter sensitivities based on the NE measure ( $F$ -value  $> 3$ ).



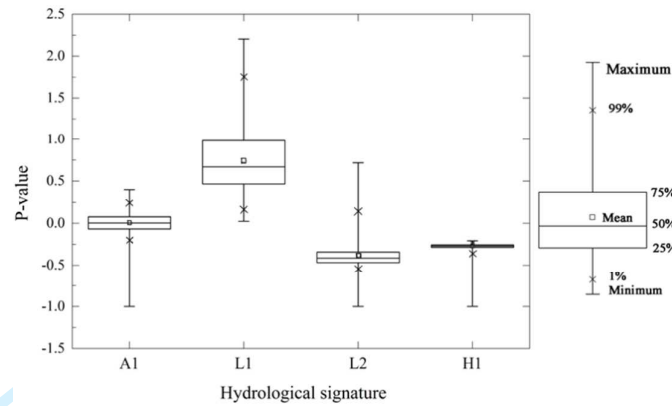
**Figure 5.** Model performance in 1994, 1995 and 1996 (corresponding to moderate, wet and dry year, respectively) when the value of  $NE$  ( $NS$ ,  $E_{rel}$  and  $NE$  are 0.83, 0.81 and 0.82 respectively) is the maximum in ANOVA sensitivity analysis.



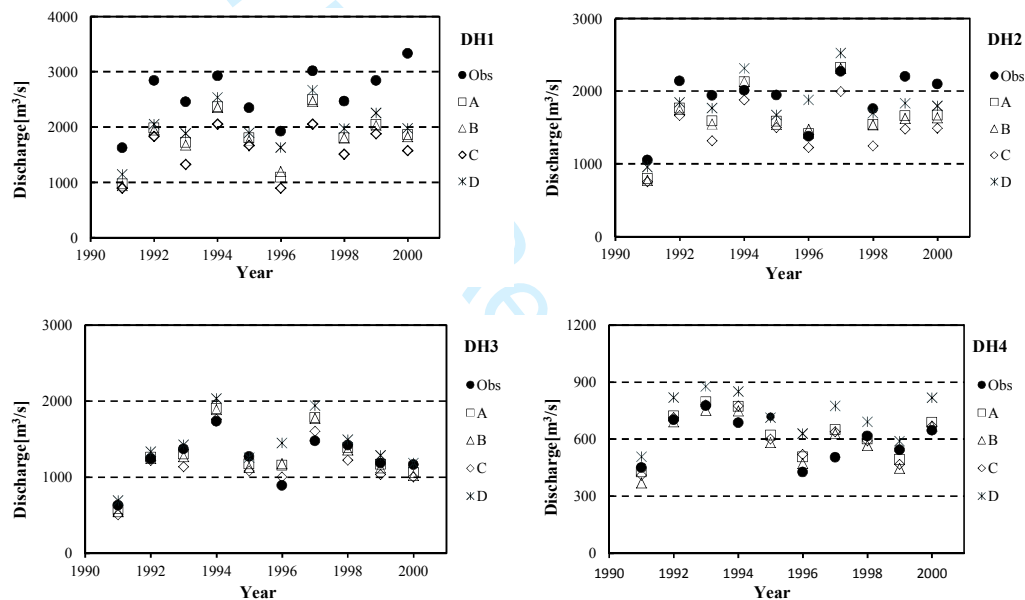
**Figure 6.** Sobol's total order sensitivity index based on the  $NE$  measure.



**Figure 7.** Interactions among sixteen parameters based on the  $NE$  measure.



**Figure 8.** Boxplot for  $P$ -value of hydrological signatures (A1 (Mean annual runoff), L1 (Low flow signature), L2 (Base-flow signature); and H1 (Specific mean annual maximum flows)) of all samples in Sobol's sensitivity analysis.



**Figure 9.** Hydrological signatures  $DH1-4$  for observed and simulated runoff from four selected samples as shown in Table 5.

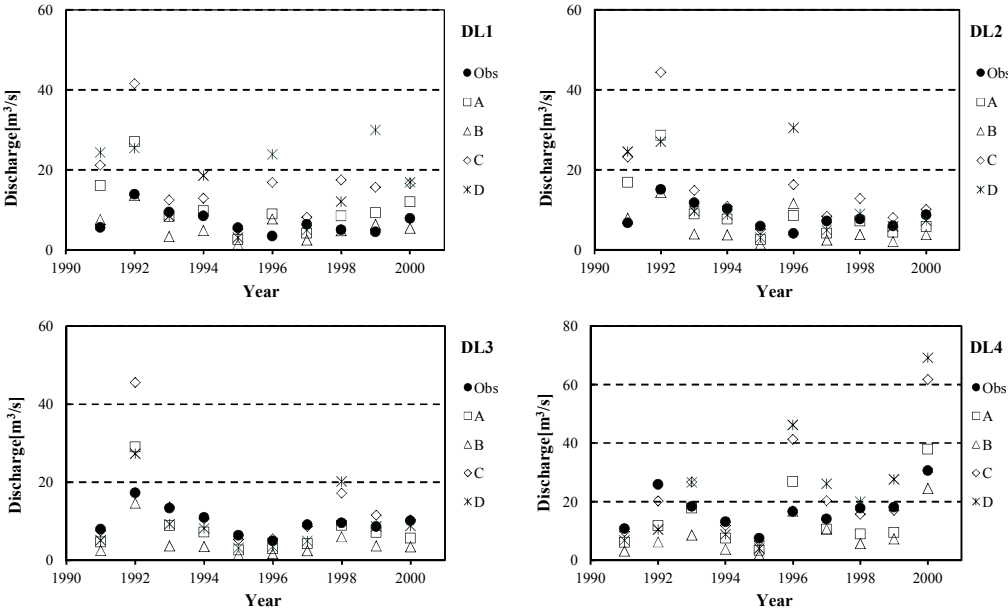


Figure 10. Hydrological signature *DLI-4* for observed and simulated runoff from four selected samples as shown in Table 5.

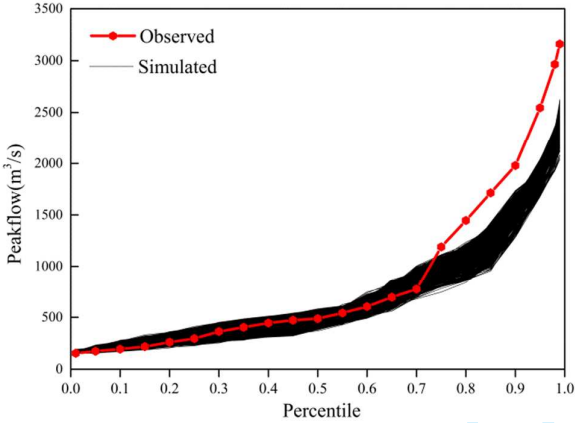


Figure 11. Peak flow percentiles for observed and simulated runoff from samples whose NS > 0.7 in Sobol's sensitivity analysis.

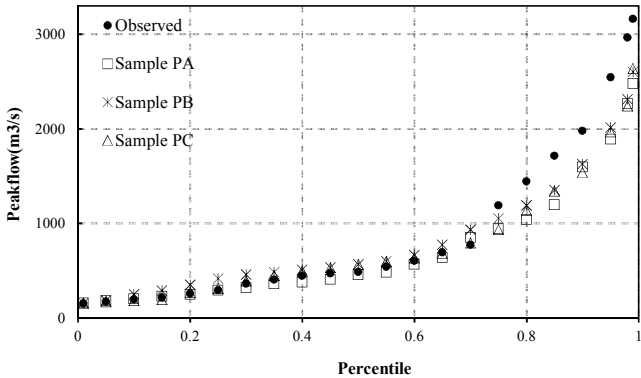


Figure 12. Peak flow percentiles for observed and simulated runoff from three selected samples as shown in Table 7.

**Table 1.** Vegetation and soil classes and their percentages in Jinhua River Basin.

Vegetation	Percentages	Vegetation	Percentages
Evergreen needleleaf forests	5.0	Water bodies	0.8
Evergreen broadleaf forests	0.1	<b>Soil</b>	<b>Percentages</b>
<i>Mixed forests</i>	29.6	<i>Sandy loam</i>	16.5
Shrublands	1.2	<i>Loam</i>	15.8
<i>Grasslands</i>	22.9	Silty clay loam	4.6
Wetlands	0.4	<i>Clay loam</i>	55.4
<i>Croplands</i>	36.7	Clay	7.3
Urban and built-up lands	3.3	Water	0.4

The italics represent soil/vegetation types whose area percentages are bigger than 10%.

**Table 2.** Ranges, unit and abbreviation of constant, soil and vegetation parameters for ANOVA sensitivity analysis.

Parameters	Abbrev.	Range	Parameters	Abbrev.	Range
<b>Constant Parameters</b>			<b>Vegetation Parameters(Grasslands, GL; Croplands, CrL)</b>		
Ground Roughness(m)	Zou	0.001~0.03	Understory Root Fraction	UFrjk	0~1
Rain Threshold(□)	Tmin	-1~0	Understory Monthly LAI(m <sup>2</sup> /m <sup>2</sup> )	ULAI	0.3~3
Reference Height(m)	Zr	30~50	Understory Monthly Alb	Uaj	0.1~0.3
Rain LAI Multiplier(m)	Rj	0.00001~0.001	Understory Height(m)	Uh	0.3~2.5
Temperature Lapse Rate(□/m)	Lt	-0.008~ 0	Maximum Resistance(s/m)	Rsmx	300~1000
<b>Vegetation Parameters( Mixed Forest, MF)</b>			Understory Minimum Resistance(s/m)	URsmin	50~300
Fractional Coverage (m <sup>2</sup> /m <sup>2</sup> )	F	0.7~1	Soil Moisture Threshold(m <sup>3</sup> /m <sup>3</sup> )	θ*	0.1~0.35
Radiation Attenuation	Lb	0.1~0.3	Vapor Pressure Deficit(pa)	Ec	1000~6000
Trunk Space(m/m)	Rt	0.4~0.6	Rpc	Rpc	10~50
Aerodynamic Attenuation	Na	1.5~3.5	Root Zone Depths(m)	D	0.1~0.8
Overstory Root Fraction	OFrjk	0~1	<b>Soil Parameters(Sandy Loam, SL; Loam, L; Clay Loam, CL)</b>		
Overstory Monthly LAI(m <sup>2</sup> /m <sup>2</sup> )	OLAI	5~10	Lateral Conductivity (m/s)	K	0.00001~0.09
Overstory Monthly Alb	Oaj	0.1~0.3	Lateral Conductivity Exponential Decrease	f	1~4
Understory Root Fraction	UFrjk	0~1	Maximum Infiltration Rate (m/s)	Imax	0.00001~0.09
Understory Monthly LAI(m <sup>2</sup> /m <sup>2</sup> )	ULAI	0.3~3	Surface Albedo (m/s)	α	0.1~0.3
Understory Monthly Alb	Uaj	0.1~0.3	Porosity(m <sup>3</sup> /m <sup>3</sup> )	φ	0.35~0.6
<i>Overstory Height(m)</i>	<i>Oh</i>	<i>10~25</i>	Pore Size Distribution	m	0.2~0.5
<i>Understory Height(m)</i>	<i>Uh</i>	<i>0.3~2.5</i>	Bubbling Pressure(m)	Ψb	0.1~0.76
Maximum Resistance(s/m)	Rsmx	2000~7000	Field Capacity(m <sup>3</sup> /m <sup>3</sup> )	θfc	0.16~0.4
<i>Overstory Minimum Resistance(s/m)</i>	<i>ORsmin</i>	<i>300~800</i>	Wilting Point(m <sup>3</sup> /m <sup>3</sup> )	θwp	0.05~0.25
<i>Understory Minimum Resistance(s/m)</i>	<i>URsmin</i>	<i>50~300</i>	Bulk Density(kg/ m <sup>3</sup> )	ρB	1000~3000
Moisture Threshold(m <sup>3</sup> /m <sup>3</sup> )	θ*	0.1~0.35	Vertical Conductivity(m/s)	Ks	0.0001~0.5
Vapor Pressure Deficit(pa)	Ec	1000~60000	Thermal Conductivity (W/mK)	Kt	3~8
Rpc	Rpc	10~50	Thermal Capacity (J/m <sup>3</sup> K)	CV	1×10 <sup>6</sup> ~ 5×10 <sup>6</sup>
Root Zone Depths(m)	D	0.1~0.8			

The abbreviations SL, L and CL in Table 2 represent sandy loam, loam and clay loam respectively. Similarly, MF, GL and CrL represent mixed forests, grasslands and croplands respectively. The italics represent parameters whose ranges for two vegetation stories are set separately.

**Table 3.** Description of the six hydrological signatures used in the study.

Conditions	Hydrological signature	Abbrev.	Unit	Definition
Average flow conditions	Mean annual runoff	<i>AI</i>	$\text{m}^3 \text{s}^{-1} \text{km}^{-2}$	Mean annual flow divided by catchment area
Low flow conditions	Low flow signature	<i>L1</i>	dimensionless	Mean of the lowest annual daily flow divided by mean annual daily flow averaged across all years
	Base-flow signature	<i>L2</i>	dimensionless	Seven-day minimum flow Divided by mean annual daily flows averaged across all years
Peak flow conditions	Specific mean annual maximum flows	<i>H1</i>	$\text{m}^3 \text{s}^{-1} \text{km}^{-2}$	Mean annual maximum flows divided by catchment area
Duration of flow events: Low flow conditions	Annual minimum of 1-/3-/7-/30-day means of daily runoff	<i>DL1-4</i>	$\text{m}^3 \text{s}^{-1}$	Magnitude of minimum annual flow of various duration, ranging from daily to monthly
Duration of flow events: Peak flow conditions	Annual maximum of 1-/3-/7-/30-day means of daily runoff	<i>DH1-4</i>	$\text{m}^3 \text{s}^{-1}$	Magnitude of maximum annual flow of various duration, ranging from daily to monthly

**Table 4.** Ranges, number and abbreviation of parameters for Sobol's sensitivity analysis.

Number	Parameters	Abbrev.	Ranges	Number	Parameters	Abbrev.	Ranges
1	Rain LAI Multiplier	Rj	0.00001-0.00	9	Understory Height(MF)	Uh(MF)	0.3-2.5
2	Wilting Point(L)	$\theta_{wp}(L)$	0.05-0.25	10	Overstory Minimum Resistance(MF)	ORsmin(MF)	300-800
3	Lateral Conductivity(CL)	K(CL)	0.00001-0.09	11	Understory Minimum Resistance(MF)	URsmin(MF)	50-300
4	Lateral (CL)	$f(CL)$	1-4	12	Understory Monthly LAI(CrL)	ULAI(CrL)	0.3-3
5	<i>Porosity(CL)</i>	$\phi(CL)$	<i>0.35-0.6</i>	13	Understory Minimum Resistance(CrL)	URsmin(CrL)	50-300
6	<i>Field Capacity(CL)</i>	$\theta_{fc}(CL)$	<i>0.16-0.4</i>	14	Soil Moisture Threshold(CrL)	$\theta^*(CrL)$	0.1-0.35
7	<i>Wilting Point(CL)</i>	$\theta_{wp}(CL)$	<i>0.05-0.25</i>	15	Vapor Pressure Deficit(CrL)	Ec(CrL)	1000-6000
8	Bulk Density(CL)	$\rho_B(CL)$	1000-3000	16	Root Zone Depths(CrL)	D(CrL)	0.1-0.8

The italics represent parameters in the Sobol's sensitivity analysis whose ranges differ from ANOVA.

**Table 5.** Selected samples based on the *NE* value.

NE	0.85-0.88	0.80-0.85	0.75-0.80	0.70-0.75
Sample	Sample A(max NE)	Sample B	Sample C	Sample D

**Table 6.** Hydrological signatures of the observed and the simulated from selected samples and corresponding *P*-values.

Hydrological Signature	Obs	Sample A		Sample B		Sample C		Sample D	
		Sim	P	Sim	P	Sim	P	Sim	P
<i>AI</i>	9.34	8.44	-0.10	7.17	-0.23	9.43	0.01	11.3	0.21
<i>L1</i>	0.05	0.08	0.68	0.05	0.07	0.11	1.37	0.092	0.97
<i>L2</i>	0.23	0.15	-0.35	0.11	-0.54	0.25	0.09	0.13	-0.42
<i>H1</i>	0.44	0.31	-0.29	0.31	-0.30	0.27	-0.39	0.34	-0.22

**Table 7.** Selected samples for peak flow based on the *NS* value.

NS	0.80-0.85	0.75-0.80	0.70-0.75
Sample	Sample PA (max NS)	Sample PB	Sample PC

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